

Statički neodređeni rešetkasti nosač

Koeficijenti uz nepoznate:

$$\delta_{ij} = \sum \frac{S_i S_j}{EF} l \rightarrow EFC \delta_{ij} = \sum S_i S_j l'' ,$$

$$\delta_{io} = \sum \frac{S_i S_o}{EF} l \rightarrow EFC \delta_{ij} = \sum S_i S_o l''$$

$$l'' = \frac{F_c}{F} l$$

$$\delta_{it} = \sum S_i \alpha_t t^\circ l \rightarrow EFC \delta_{ij} = EFC \sum S_i \alpha_t t^\circ l$$

$$\delta_{i\alpha} = \delta_{io} + \delta_{it} + \delta_{ic}$$

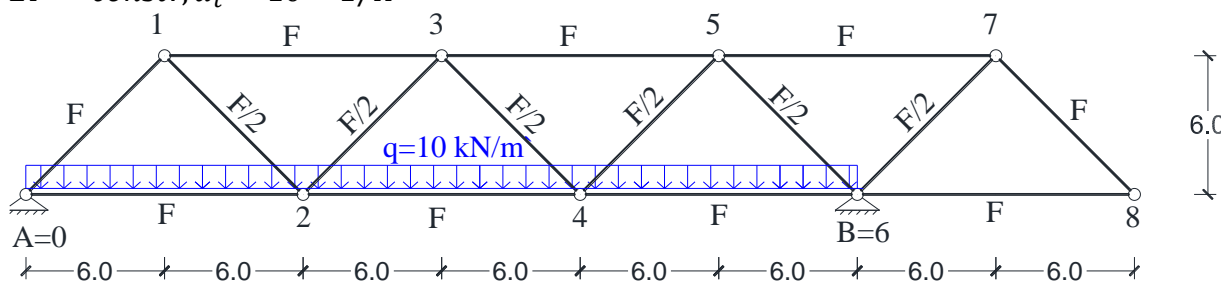
$$\delta_{ic} = - \sum C_i c_i \rightarrow EFC \delta_{ij} = -EFC \sum C_i c_i$$

Zadatak: Za dati rešetkasti nosač prema skici odrediti vertikalno pomeranje čvora "8" usled:

a) Datog opterećenja

b) Zagrevanja štapova gornjeg pojasa za 20K

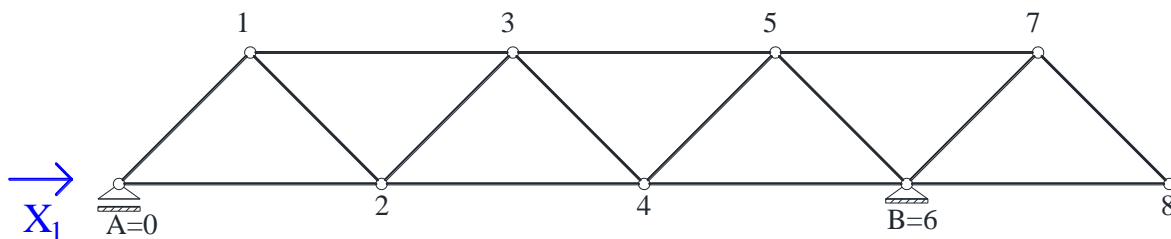
$$EF = \text{const.}, \alpha_t = 10^{-5} 1/K$$



1. Statička neodređenost

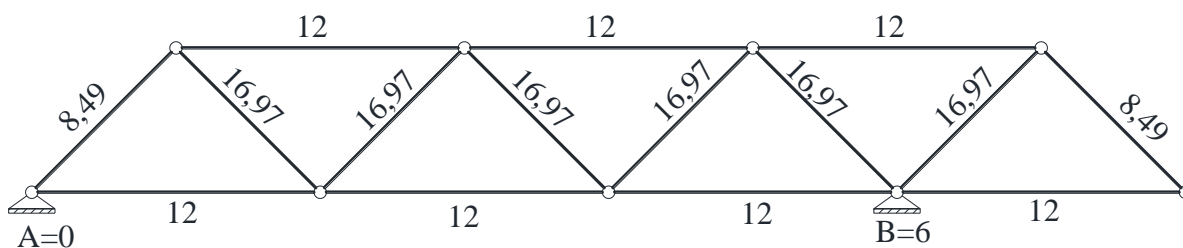
$$Z_o=4, Z_s=15, K=9, n = Z_s + Z_o - 2K = 1 \text{ x stat. neod. nosač}$$

2. Osnovni sistem



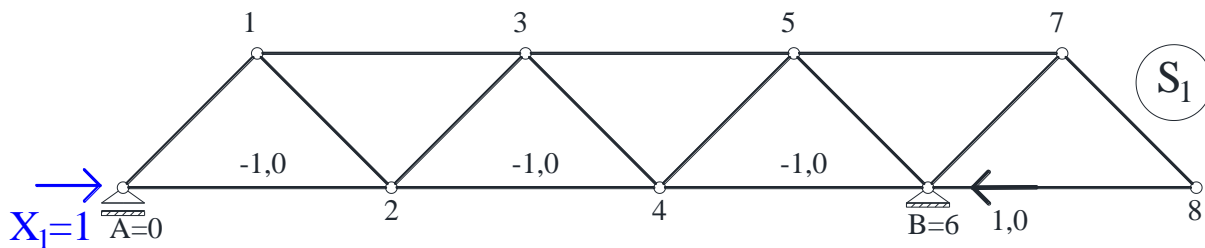
3. Redukovane dužine

$$F_c = F, l'' = \frac{F_c}{F} l$$



STATIKA KONSTRUKCIJA 1 - VEŽBE

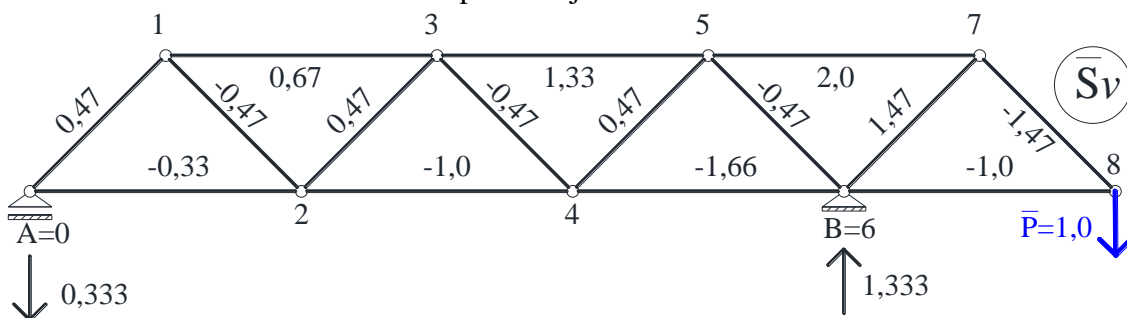
4. Sile u štapovima za stanje $X_1=1,0$



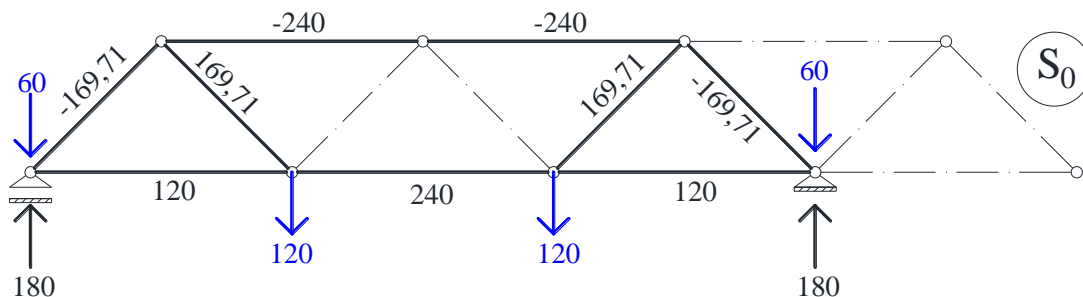
5. Koeficijenti uz nepoznate

$$EFc\delta_{11} = \sum S_1 S_1 l'' = 3 \cdot (-1) \cdot (-1) \cdot 12 = 36,0$$

6. Generalisana sila za vertikalno pomeranje



a) Pomeranje čvora "8" usled zadatog opterećenja



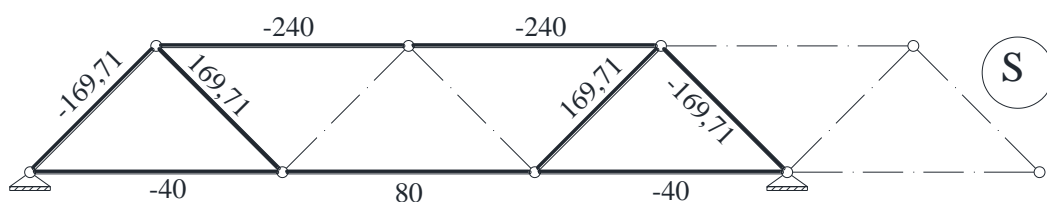
-Slobodni članovi

$$EFc\delta_{10} = \sum S_1 S_0 l'' = 2 \cdot (-1) \cdot 120 \cdot 12 + (-1) \cdot 240 \cdot 12 = -5760$$

-Statički neodređena veličina

$$X_1 = -\frac{\delta_{10}}{\delta_{11}} = \frac{5760}{36} = 160 \text{ kN}$$

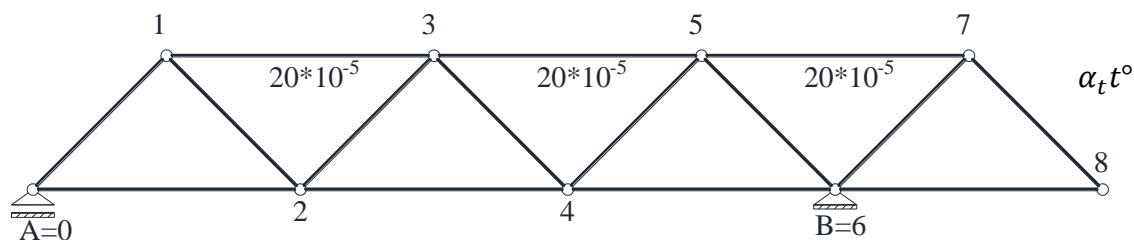
-Sile u štapovima $S = S_0 + S_1 X_1$



STATIKA KONSTRUKCIJA 1 - VEŽBE

$$\begin{aligned}
 EFcv_8 &= \sum S\bar{S}_v l'' \\
 &= 12 \cdot [-240(0,67 + 1,33) - 40(-0,33 - 1,67) - 1 \cdot 80] + 8,49(-169,71) \\
 &\quad \cdot 0,47 + 16,97[-0,47(169,71 - 169,71 - 169,71)] = -5083,60
 \end{aligned}$$

b) Pomeranje čvora "8" usled temperaturne promene



-Slobodni članovi

$$EFc\delta_{1t} = EFc \sum S_1 \alpha_t t^\circ l = 0$$

-Statički neodređena veličina

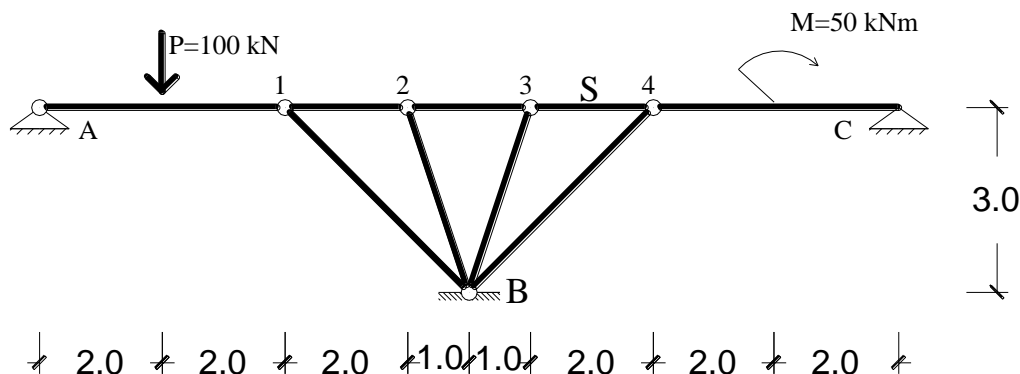
$$X_{1,t} = -\frac{\delta_{1t}}{\delta_{11}} = 0$$

-Sile u štapovima $S_t = S_1 X_{1,t} = 0$

$$v_8 = \sum \frac{S_t \bar{S}_v}{EF} l + \sum \bar{S}_v \alpha_t t^\circ l = 12 \cdot 20 \cdot 10^{-5} (0,66 + 1,33 + 2) = 0,0096m$$

Zadatak: Za nosač na slici odrediti obrtanje štapa "S" usled jednovremenog delovanja datog opterećenja i pomeranja oslonca "C" u levo za 5cm.

Geometrijske karakteristike: grede A-1 i 4-C: 20/40cm
ostali štapovi: 20/20cm
 $E = 3 \cdot 10^7 \text{ kN/m}^2$.

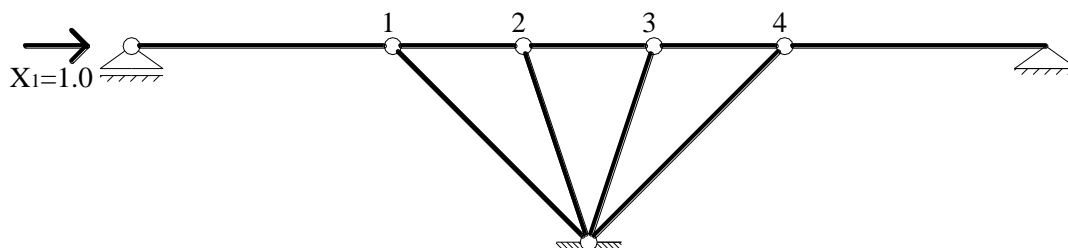


STATIKA KONSTRUKCIJA 1 - VEŽBE

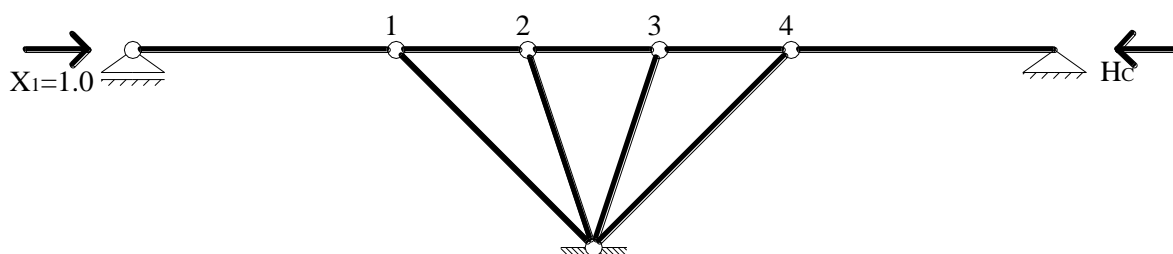
- Statička neodređenost nosača

$$n = Z_s + Z_k + Z_o + Z_u - 2K = 9 + 0 + 6 + 0 - 2 \cdot 7 = 1 \text{ x stat. neodređen nosač}$$

-Izbor osnovnog sistema



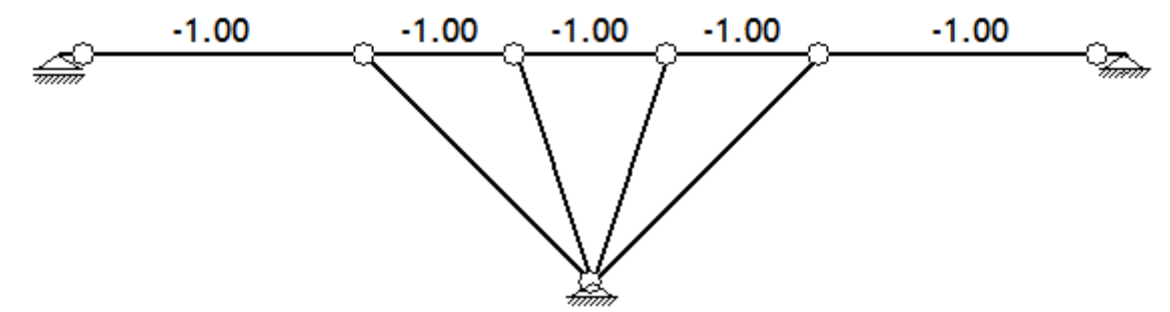
-Reakcije oslonaca usled statički nepoznate $X_1=1.0$



1. $\sum M_1^l = 0 \rightarrow A = 0$
2. $\sum M_4^d = 0 \rightarrow C = 0$
3. $\sum M_B = 0 \rightarrow H_C = 1.0$
4. $\sum H_i = 0 \rightarrow H_B = 0$
5. $\sum V_i = 0 \rightarrow B = 0$

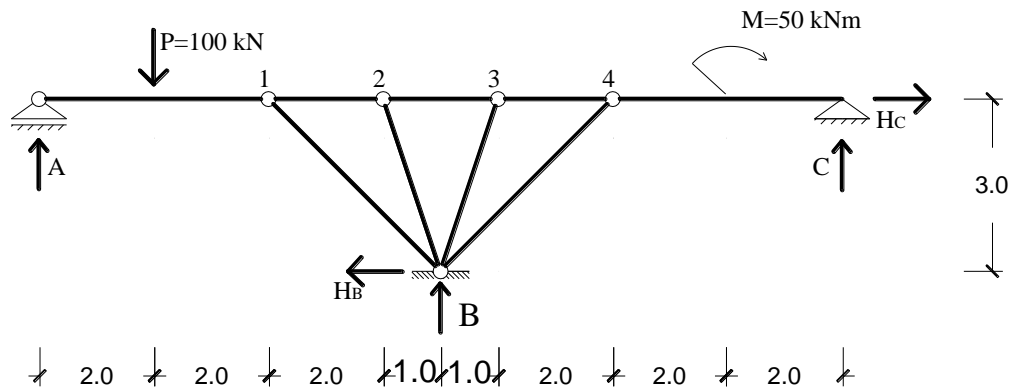
Opterećenje na osnovnom sistemu ne izaziva transverzalne sile i moment savijanja.

- Dijagram normalnih sila (N_1)



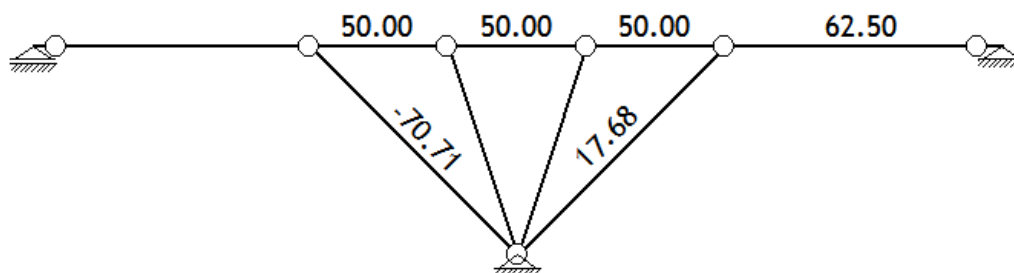
STATIKA KONSTRUKCIJA 1 - VEŽBE

-Reakcije oslonaca na osnovnom sistemu usled zdatog opterećenja



1. $\sum M_1^l = 0 \rightarrow A = 50 \text{ kN}$
2. $\sum M_4^d = 0 \rightarrow C = 12.5 \text{ kN}$
3. $\sum M_B = 0 \rightarrow H_C = 62.5 \text{ kN}$
4. $\sum H_i = 0 \rightarrow H_B = 62.5 \text{ kN}$
5. $\sum V_i = 0 \rightarrow B = 37.5 \text{ kN}$

-Dijagram normalnih sila usled zdatog opterećenja (N_o [kN])



-Geometrijske karakteristike

$$F_c = 0.2 \cdot 0.2 = 0.04 \text{ m}^2, I_c = 0.2 \cdot \frac{0.2^3}{12} = 1.33 \cdot 10^{-4} \text{ m}^4, \frac{I_c}{F_c} = 3.33 \cdot 10^{-3} \text{ m}^2, EI_c = 4000 \text{ kNm}^2$$

-Uslovna jednačina metode sila

$$\delta_{10} + \delta_{1c} + \delta_{11}X_1 = 0$$

$$EI_c \delta_{10} = \frac{I_c}{F_c} \int N_1 N_0 \frac{F_c}{F} ds = 3.33 \cdot 10^{-3} [-1 \cdot 50(2 + 2 + 2) - 1 \cdot 62.5 \cdot 2] = -1.417$$

$$EI_c \delta_{1c} = -EI_c \sum \bar{c}_i c_i = -4000 \cdot 1 \cdot 0.05 = -200$$

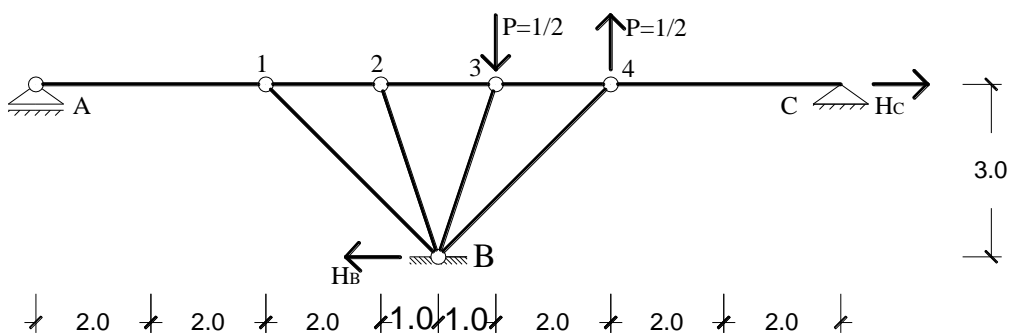
$$EI_c \delta_{11} = \frac{I_c}{F_c} \int N_1 N_1 \frac{F_c}{F} ds = 3.33 \cdot 10^{-3} [1^2(2 + 2 + 2 + 2 + 2)] = 0.03333$$

-Uslovna jednačina metode sila

$$\delta_{10} + \delta_{1c} + \delta_{11}X_1 = 0 \rightarrow X_1 = \frac{201.42}{0.0333} = 6042.66 \text{ kN}$$

STATIKA KONSTRUKCIJA 1 - VEŽBE

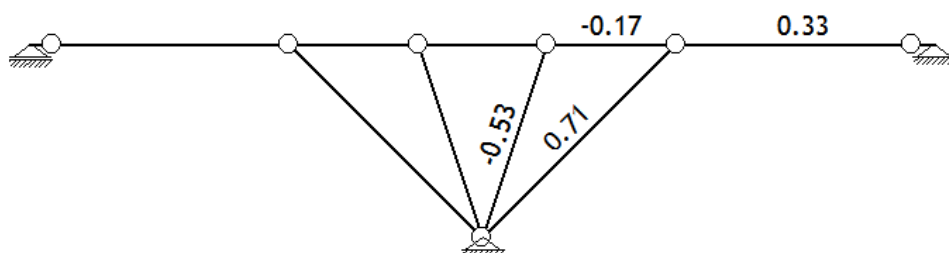
-Uticaji na nosaču usled generalisane sile za obrtanje štapa "S"



1. $\sum M_1^l = 0 \rightarrow A = 0$
2. $\sum M_4^d = 0 \rightarrow C = 0$
3. $\sum M_B = 0 \rightarrow H_C = 0.33$
4. $\sum H_i = 0 \rightarrow H_B = 0.33$
5. $\sum V_i = 0 \rightarrow B = 0$

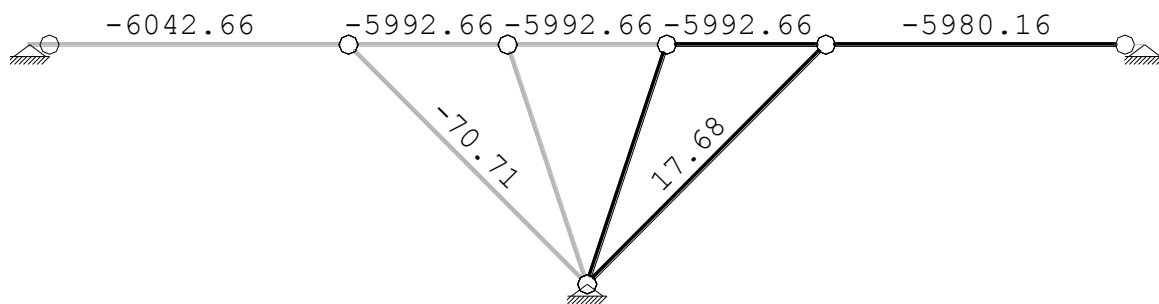
Generalisano opterećenje na osnovnom sistemu ne izaziva transverzalne sile i moment savijanja.

- Dijagram normalnih sila usled generalisane sile (\bar{N})



- Dijagram normalnih sila na zatom statički neodređenom nosaču (N[kN])

$$Z = Z_0 + Z_1 X_1$$



-Obrtanje štapa S

$$EI_c \phi = \frac{I_c}{F_c} \int N \bar{N} \frac{F_c}{F} d_s - EI_c \sum \bar{c}_i c_i$$

$$= 3.33 \cdot 10^{-3} [17.68 \cdot 0.71 \cdot 4.24 + 5992.66 \cdot 0.17 \cdot 2 - 5980.16 \cdot 0.33 \cdot 2] + 4000 \cdot 0.33 \cdot 0.05 = 60,35$$